

# Novel approaches to estimating turbulent EDR from low and moderate resolution velocity time series

Marta Waławczyk<sup>1</sup>, Yong-Feng Ma<sup>1</sup>, Jacek M.Kopec<sup>1,2</sup>, Emmanuel O. Akinlabi<sup>1</sup>, Szymon P. Malinowski<sup>1</sup>

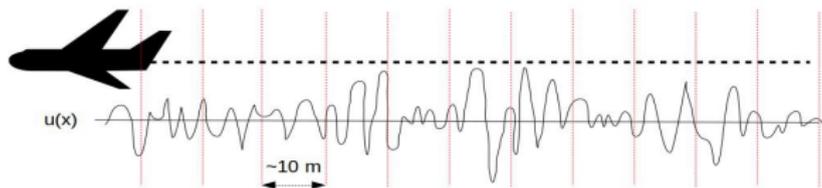
<sup>1</sup> *Institute of Geophysics, Faculty of Physics, University of Warsaw (UW), Poland*

<sup>2</sup> *Interdisciplinary Centre of Mathematical and Numerical Modelling, UW, Poland*

Experiments in Fluid Mechanics, Warsaw, 23-24.10.2017

## Motivation

- Information on turbulent kinetic EDR based on in-situ airborne measurements is still scarce.
- Research aircraft are often not equipped to measure wind fluctuations with spatial resolution better than few tens of meters
- Estimates of  $\epsilon$  at such low resolutions using power spectral density or structure functions are complex and far from being standardised



## Motivation

Can we introduce alternative methods to increase robustness of  $\epsilon$  retrievals?



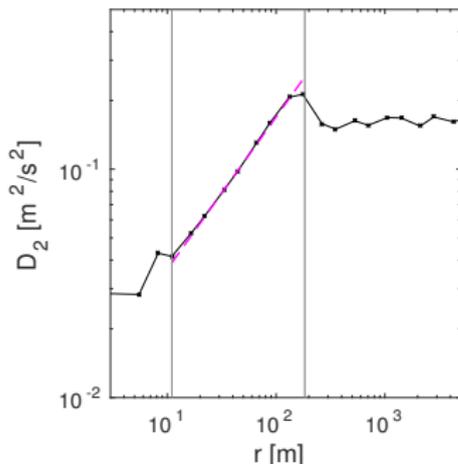
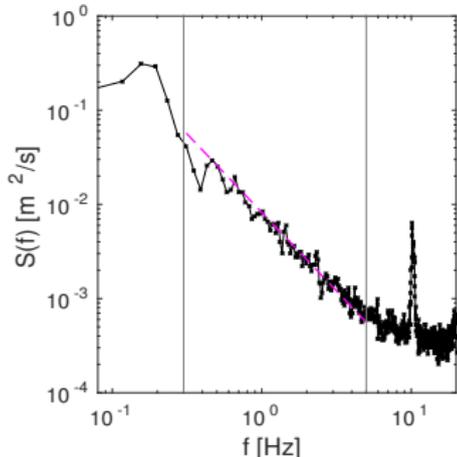
Kopeć, J.M., Kwiatkowski, K., de Haan, S. and Malinowski, S.P.: Retrieving atmospheric turbulence information from regular commercial aircraft using Mode-S and ADS-B, *Atmos. Meas. Tech.*, **9**, 2016



## Existing methods for $\epsilon$ retrieval

Inertial-range scaling of power spectral density and 2<sup>nd</sup>-order structure function  $C_1 \approx 0.49$ ,  $C_2 \approx 2$ .

$$S(f) = C_1 \left( \frac{U}{2\pi} \right)^{2/3} \epsilon^{2/3} f^{-5/3}, \quad D_2(r) = C_2 \epsilon^{2/3} r^{2/3}.$$



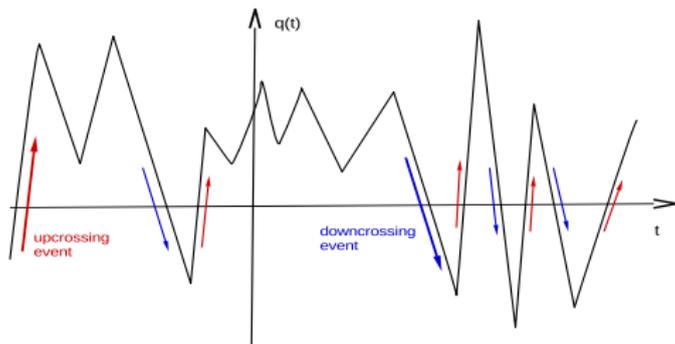
## Existing methods for $\epsilon$ retrieval

### Method based on the number of zero-crossings

Rice [Bell. Syst. Tech. J., **24**, 1945]

$$N^2 = \frac{\langle (\partial u' / \partial x)^2 \rangle}{\pi^2 \langle u'^2 \rangle}.$$

$N$  - number of zero-crossings per unit length



## Existing methods for $\epsilon$ retrieval

### Method based on the number of zero-crossings

$$\epsilon = 15\nu \left\langle \left( \frac{\partial u'}{\partial x} \right)^2 \right\rangle = 15\nu \frac{\langle u'^2 \rangle}{\lambda_n^2} \quad \lambda_n \text{-Taylor microscale}$$

Sreenivasan et al. [J. Fluid Mech., 137, 1983]

$$N^2 = \frac{\langle (\partial u' / \partial x)^2 \rangle}{\pi^2 \langle u'^2 \rangle} \implies \epsilon = 15\pi^2 \nu u'^2 N^2$$

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Method based on the number of zero-crossings can be used for signals resolved down to the smallest dissipative eddies...

...which is not the case for airborne velocity measurements.

New proposal: Reformulation of the original zero-crossing method in order to estimate  $\epsilon$  from  $N$  of signals with spectral cut-off.

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**New proposal:** Reformulation of the original zero-crossing method in order to estimate  $\epsilon$  from  $N$  of signals with spectral cut-off.

## New proposals

$N$  is related to the dissipation spectra  $\sim 2\nu f^2 S(f)$ :

$$u'^2 N^2 = 4 \int_0^\infty f^2 S(f) df \quad \text{and} \quad u'_{cut}{}^2 N_{cut}^2 = 4 \int_0^{f_{cut}} f^2 S(f) df$$

$u'_{cut}$ ,  $N_{cut}$  calculated for a signal with spectral cut-off at  $f_{cut}$ .  
In the inertial range  $S(f) = C_1 (U/2\pi)^{2/3} \epsilon^{2/3} f^{-5/3}$ . Subtracting equations for two different  $f_{cut}$ ,  $f_1 < f_2$  from the inertial range

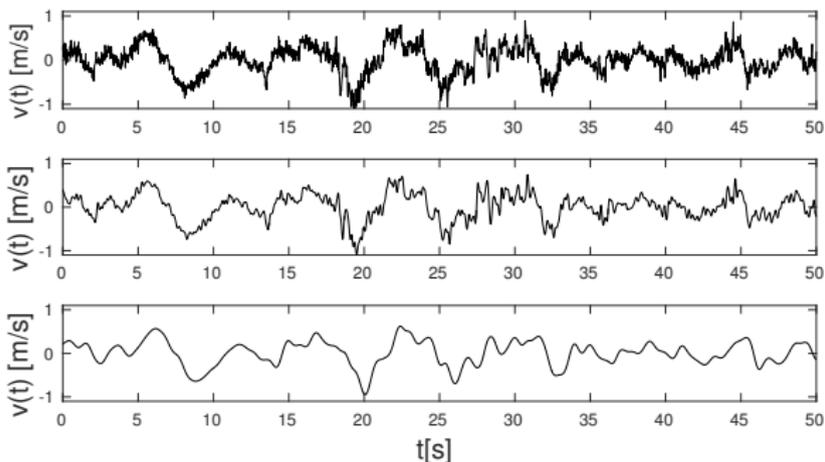
$$(u_2'^2 N_2^2 - u_1'^2 N_1^2) = 3C_1 \left(\frac{U}{2\pi}\right)^{2/3} \epsilon^{2/3} (f_2^{4/3} - f_1^{4/3}).$$

Waclawczyk M., Ma Y.-F., Kopeć J., Malinowski S. P. Novel approaches to estimating turbulent kinetic energy dissipation rate from low and moderate resolution velocity fluctuation time series, Atmos. Meas. Tech. Discuss., 2017



## New proposals

Successive filtering of a signal with  $f_1 < f_2 < \dots < f_i < \dots$



For each signal with cut-off  $f_i$  we calculate the number of zero-crossings per unit time  $N_i$



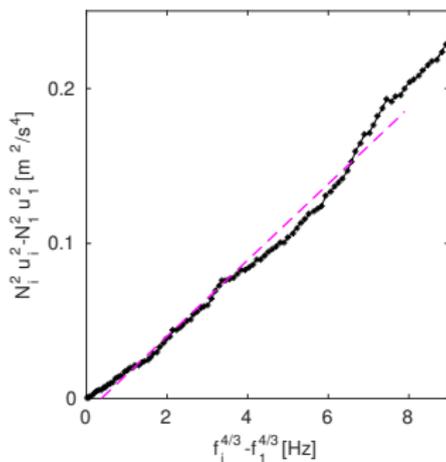
## New proposals

$$(u_2'^2 N_2^2 - u_1'^2 N_1^2) = 3C_1 \left( \frac{U}{2\pi} \right)^{2/3} \epsilon^{2/3} (f_2^{4/3} - f_1^{4/3}).$$

With linear curve-fitting

$$3C_1 \left( \frac{U}{2\pi} \right)^{2/3} \epsilon^{2/3}$$

is estimated and the corresponding value of  $\epsilon$  is found



## New proposals

Second proposal: Recovering the missing part of the spectrum

$$u'^2 N^2 = u'_{cut}{}^2 N_{cut}^2 \frac{\int_0^\infty k_1^2 E_{11} dk_1}{\int_0^{k_{cut}} k_1^2 E_{11} dk_1} = u'_{cut}{}^2 N_{cut}^2 \left( 1 + \frac{\int_{k_{cut}}^\infty k_1^2 E_{11} dk_1}{\int_0^{k_{cut}} k_1^2 E_{11} dk_1} \right)$$

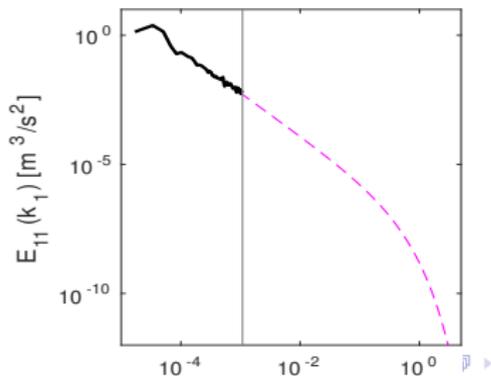
assume certain form of the energy spectrum

[Pope, *Turbulent flows*, 2001]

$$E(k) = C\epsilon^{2/3} k^{-5/3} f_\eta(\beta k \eta),$$

with ( $\beta = 5.2$  and  $c_\eta = 0.4$ )

$$f_\eta = e \left\{ -[(\beta k \eta)^4 + (\beta c_\eta)^4]^{1/4} + \beta c_\eta \right\}$$



## New proposals

Next, use relation between  $E(k)$  and  $E_{11}(k_1)$ , to finally arrive at

$$u'^2 N^2 \approx u'_{cut}{}^2 N_{cut}^2 \underbrace{\left[ 1 + \frac{\int_{k_{cut}\beta\eta}^{\infty} \xi_1^2 \int_{\xi_1}^{\infty} \xi^{-8/3} f_{\eta}(\xi) \left(1 - \frac{\xi_1^2}{\xi^2}\right) d\xi d\xi_1}{\int_0^{k_{cut}\beta\eta} \xi_1^2 \int_{\xi_1}^{\infty} \xi^{-8/3} f_{\eta}(\xi) \left(1 - \frac{\xi_1^2}{\xi^2}\right) d\xi d\xi_1} \right]}_{\mathcal{C}_{\mathcal{F}}}$$

$$u'^2 N^2 = u'_{cut}{}^2 N_{cut}^2 \mathcal{C}_{\mathcal{F}},$$

where  $\mathcal{C}_{\mathcal{F}}$  is a correcting factor to be calculated

$$\epsilon = 15\pi^2 \nu u'_{cut}{}^2 N_{cut}^2 \mathcal{C}_{\mathcal{F}}$$

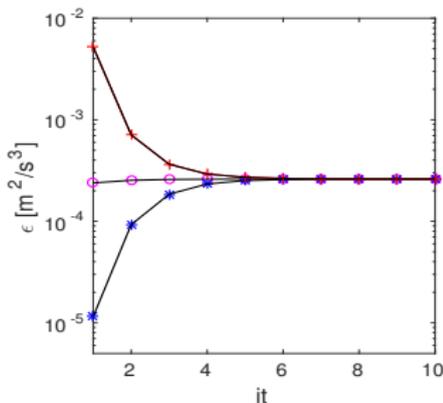


## New proposals

The integral bounds contain the Kolmogorov scale  $\eta = (\nu^3/\epsilon)^{1/4}$

### Iterative procedure:

- Calculate  $u_{cut}'^2 N_{cut}^2$  of a signal
- Guess first value  $\epsilon^0, \eta^0 = (\nu^3/\epsilon^0)^{1/4}$
- Calculate  $C_{\mathcal{F}}$
- Calculate  $\epsilon^1 = 15\pi^2 \nu u_{cut}'^2 N_{cut}^2 C_{\mathcal{F}}$
- Repeat the procedure

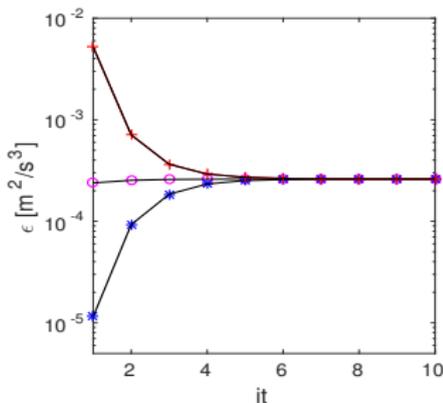


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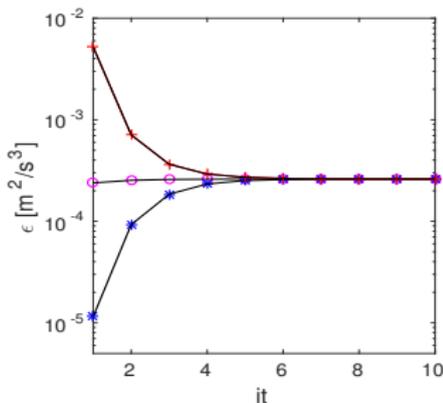


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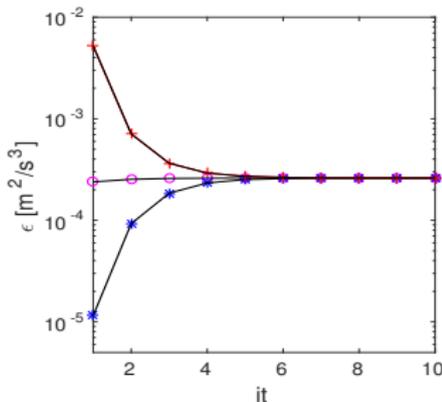


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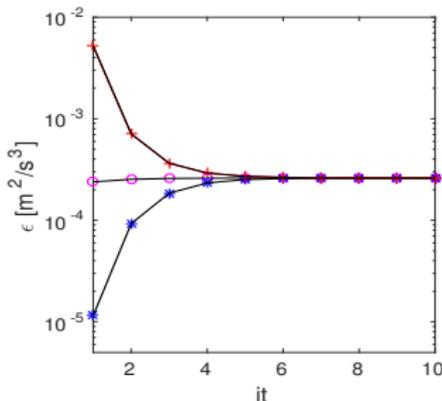


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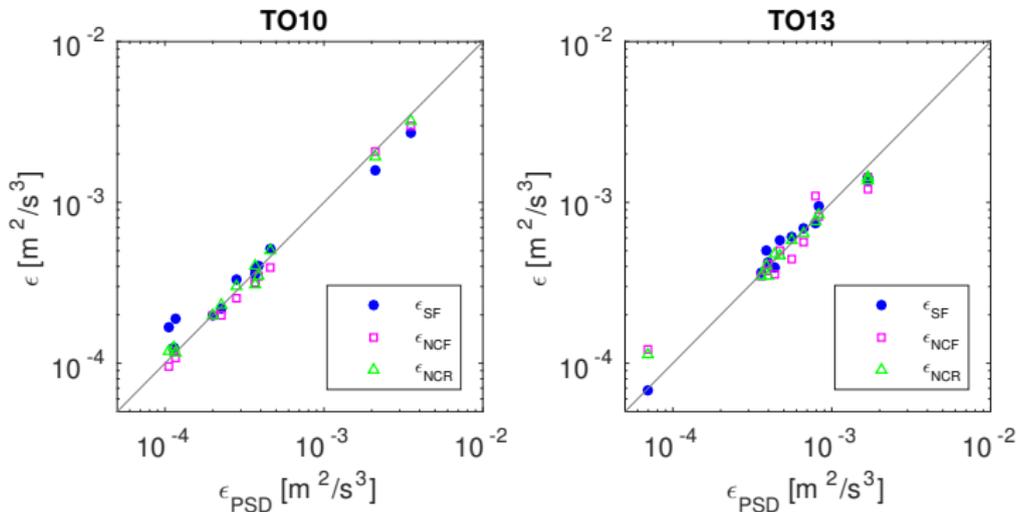
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## Results - POST measurements

### POST research campaign flights TO10 and TO13

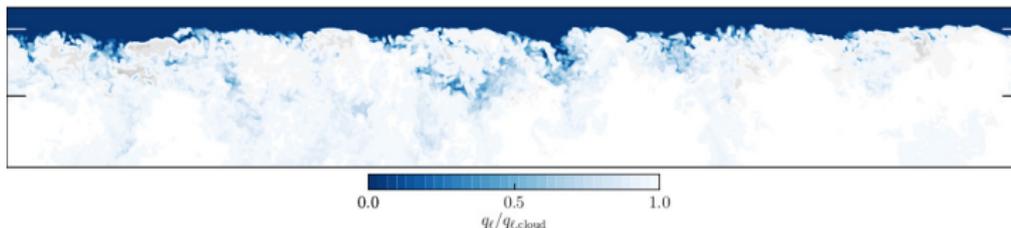
La Plante et al.: Physics of Stratocumulus Top (POST): turbulence characteristics, Atmos. Chem. Phys., **16**, 2016.



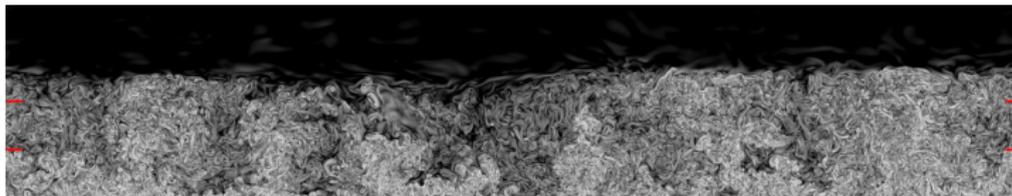
## Results - DNS data

courtesy of Prof. J.-P. Mellado from the Max Planck Institute for Meteorology

### stratocumulus cloud-top simulations



### free convection



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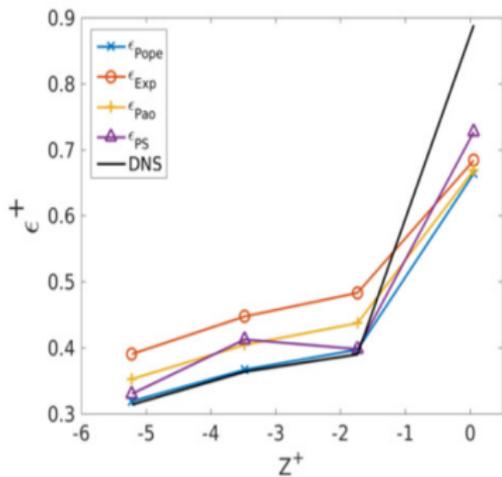


Figure: Stratocumulus cloud-top

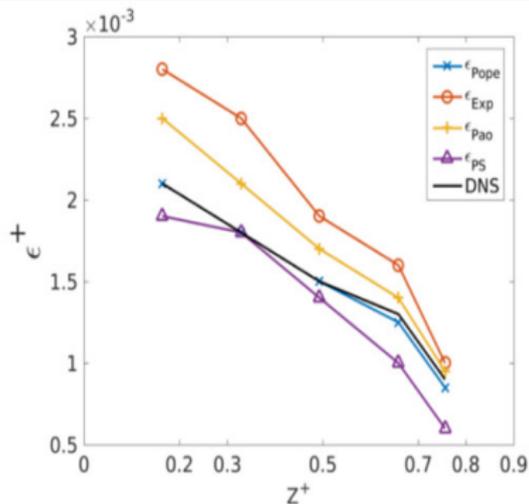


Figure: Free convection

## Conclusions

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- Two new methods for  $\epsilon$  retrieval using number of crossings per unit length were proposed.
- Possible advantages are:
  - Increased robustness of  $\epsilon$  retrieval
  - New methods seem to be less sensitive to bias errors due to finite averaging windows
  - Second method - can be used for signals with large part of the dissipative spectrum resolved
- Disadvantages
  - Possibly larger scatter of results (at least in the case of artificial velocity fields)
  - Additional assumptions needed (Gaussianity of the process)

## Acknowledgements

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The financial support of the National Science Centre, Poland ([project No. 2014/15/B/ST8/00180](#) and [2016/21/B/ST8/01010](#)) is gratefully acknowledged. The POST field campaign was supported by US National Science Foundation through grant [ATM-0735121](#) and by the Polish Ministry of Science and Higher Education through grant [186/W-POST/2008/0](#).

## New proposals

### Iterative procedure:

- Calculate  $U_{cut}^2 N_{cut}^2$  of a signal

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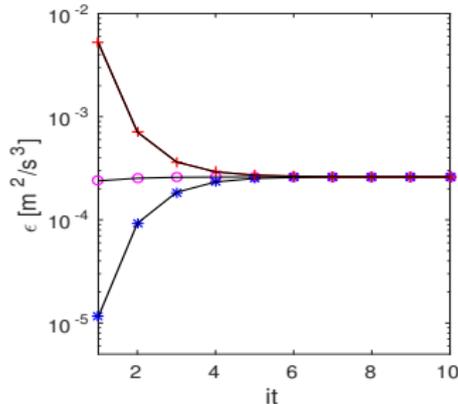
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- Calculate  $C_{\mathcal{F}} =$

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- Calculate  $\epsilon^1 = 15\pi^2 \nu U_{cut}^2 N_{cut}^2 C_{\mathcal{F}}$

- Repeat the procedure



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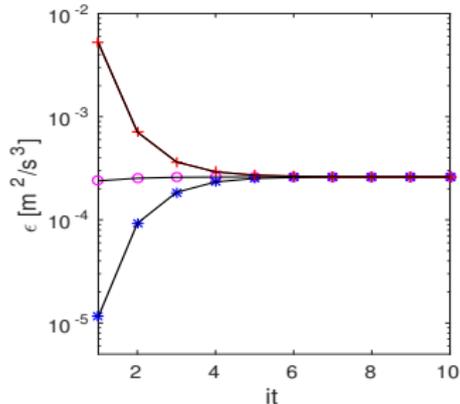
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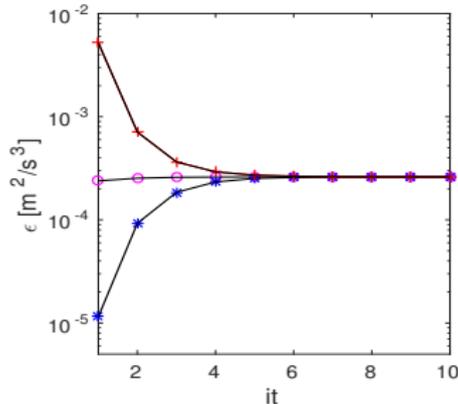
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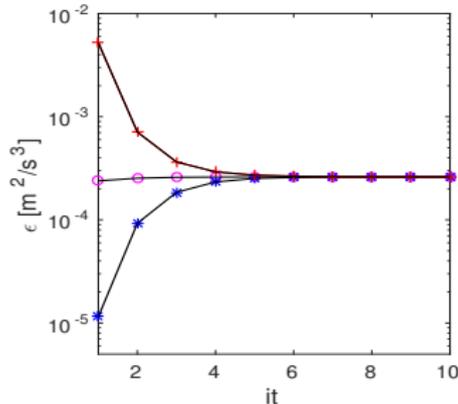
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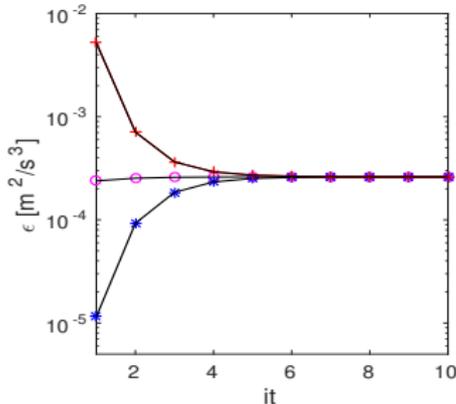
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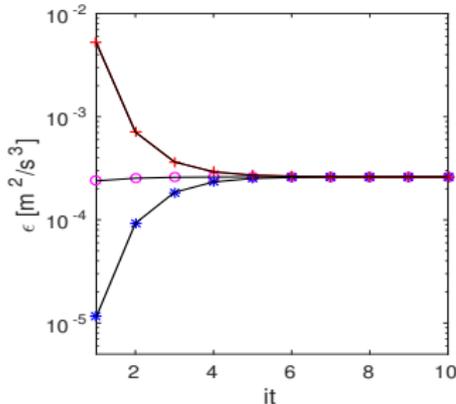
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## Results - artificial velocity fields

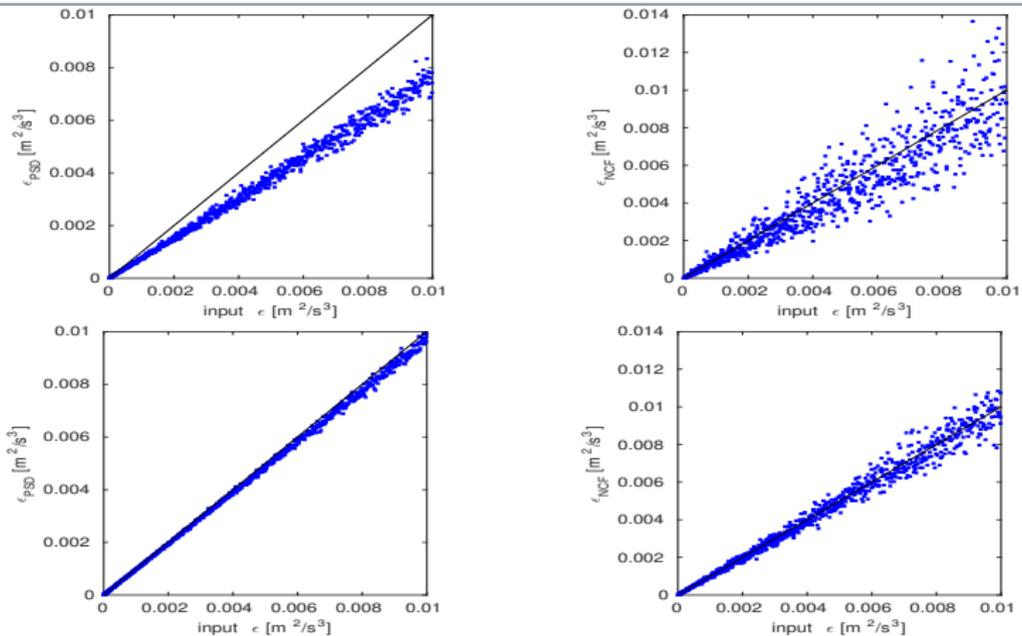


Figure: Estimated values of  $\epsilon_{PSD}$  and  $\epsilon_{NCF}$  for the 200 Hz synthetic signals and fitting range 1 – 20 Hz as functions of corresponding input  $\epsilon$  for upper plots: signals with  $L \approx 50L_0$ , lower plots: signals with  $L \approx 400L_0$ .